

# Parabolized Navier-Stokes Analysis of Three-Dimensional Supersonic and Subsonic Jet Mixing Problems

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## Abstract

**P**ARABOLIZED Navier-Stokes (PNS) models under development for the analysis of three-dimensional supersonic and subsonic propulsive jet mixing problems are described herein. The supersonic model, SCIP3D, is a direct extension of the 2D SCIPVIS PNS model of Dash and Wolf. It analyzes over- or underexpanded single and multiple rectangular jets employing a shock-capturing formulation. In the subsonic model, SPLIT3D, spatial marching capabilities are achieved via a pressure-splitting approximation and an extension of the two-dimensional noniterative cross-flow procedure of Dash and Sinha to three-dimensional flows. Both models contain  $k\epsilon$  and  $kW$  two-equation turbulence model formulations and permit analyzing nonreacting multi-component gas mixtures. Numerical studies are presented which demonstrate both codes' current capabilities.

## Contents

The analysis of aircraft propulsive jets issuing from nonaxisymmetric nozzles requires the use of supersonic shock-capturing PNS methodology to treat the inner, shock-dominated region of the jet and subsonic pressure-split PNS methodology to treat the outer, vortex-entrainment dominated region for subsonic flight velocities. The ability to treat two-dimensional/axisymmetric jet problems using spatial marching PNS methodology has been demonstrated in recent publications by the authors. The SCIPVIS shock-capturing model of Dash and Wolf<sup>1,2</sup> treats the complex interactions between shock and turbulent mixing processes in supersonic jets.<sup>3,4</sup> The SPLITP model of Dash and Sinha<sup>5,6</sup> employs a pressure-splitting approach to treat subsonic jet mixing problems using a noniterative procedure<sup>7</sup> to treat pressure/cross flow velocity coupling in the cross flow plane. This paper describes preliminary extensions of SCIPVIS and SPLITP methodology to three-dimensional jet mixing problems as embodied in the SCIP3D and SPLIT3D models.

## Three-Dimensional PNS Jet Equations

The conservation form of the three-dimensional PNS equations governing rectangular jet mixing are

$$\frac{\partial \bar{E}}{\partial x} + \frac{\partial \bar{F}}{\partial y} + \frac{\partial \bar{G}}{\partial z} = \bar{V}_f \quad (1)$$

where

$$\bar{f} = [1, U, V, W, H, \phi]^T$$

$$\bar{E} = \rho U [1, P/\rho U + U, V, W, H, \phi]^T$$

$$\bar{F} = \rho V [1, U, P/\rho V + V, W, H, \phi]^T$$

$$\bar{G} = \rho W [1, U, V, P/\rho W + W, H, \phi]^T$$

and the parabolized stress terms  $\bar{V}_f$ , are described in the full paper.

## Supersonic PNS Model, SCIP3D

The mean flow and turbulence model equations are solved in mapped rectangular coordinates using a rotating version of the explicit MacCormack algorithm. The computational grid (Fig. 1) initially encompasses the viscous jet and the jet-induced interaction flowfield. For problems with quarter-plane symmetry, the initial spanwise and vertical boundary growth  $[Y_u(x)$  and  $Z_u(x)]$  is based on exact alignment of the viscous dividing streamlines in the symmetry planes with mapped coordinate lines. This minimizes numerical diffusion effects in the thin near-field shear layer region. Downstream, the computational boundary growth is adaptive and keyed to viscous edge gradients, transitioning from rectangular to square as the jet takes on a circular appearance. The captured plume induced bow shock ultimately exits the computational domain; downstream, one-wave flow relations are utilized permitting waves to exit the flow with no reflections back into the computational domain. Details are provided in the full paper.

A number of calculations are described in the full paper for square and rectangular (4/1 aspect ratio), balanced pressure and underexpanded ( $P_j/P_e = 2/1$ ) hot Mach 3 jets ( $U_j = 8820$  ft/s,  $T_j = 2000^\circ\text{K}$ ) exhausting into a Mach 3 uniform external stream ( $U_e = 4410$  ft/s,  $T_e = 500^\circ\text{K}$ ). Calculations are also described for the an infinite array of square underexpanded jets having the above conditions. Figure 2 exhibits a schematic of the multiple jet calculation and the predicted wave/shear layer structure and pressure contours in the  $Z=0$  symmetry plane.

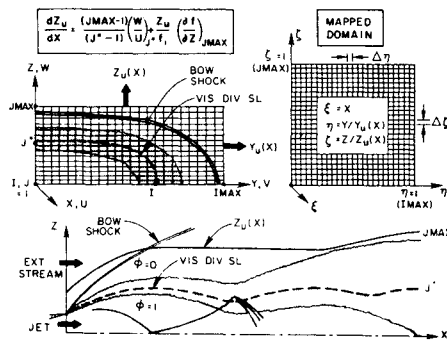
## Subsonic PNS Model, SPLIT3D

In subsonic applications, the pressure field is "split" with the axial pressure gradient specified, and the cross-flow pressure variation determined via a coupled solution of the continuity and cross-flow momentum equations. The step-wise marching solution is comprised of a "parabolic" solution of Eq. (1) (achieved by treating the pressure gradient term in the axial momentum as a known source term, and using an upwind variant of the MacCormack predictor/corrector algorithm in the outer, entrainment dominated region of the jet) followed by a cross-flow solution. Previous cross-flow solutions have often exhibited convergence problems due to the strong coupling of the  $V$  and  $W$  velocity components in vortical-corner regions. In the approach developed here, the noniterative two-dimensional cross flow procedure of Dash and Sinha<sup>7</sup> is extended to the three-dimensional cross flow problem leading to a system of coupled equations for  $V$  and  $W$  which are solved concurrently

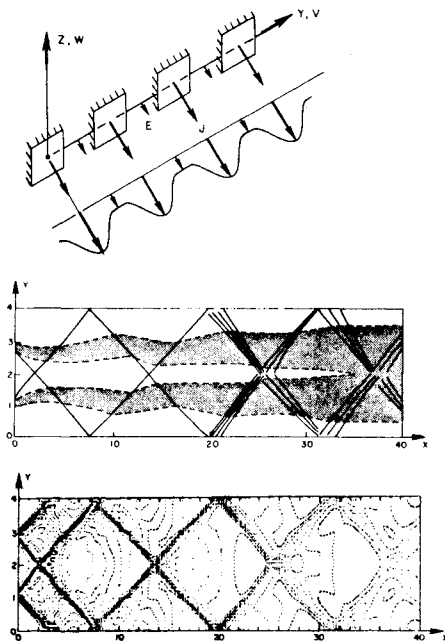
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**Fig. 1 Grid nomenclature, boundary growth formulation, and mapped computational domain utilized in SCIP3D model.**

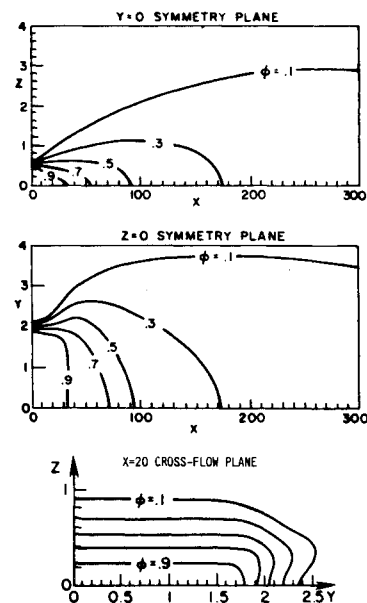


**Fig. 2 Schematic of supersonic multiple square jet problem and predicted flow pattern and pressure contours in  $Z=0$  symmetry plane.**

with the pressure field lagged. The details are given in the full paper.

A series of SPLIT3D calculations were performed to analyze subsonic square and rectangular jets exhausting into a uniform subsonic external stream. All calculations simulated the parallel mixing of a Mach 0.26 jet exhausting into a Mach 0.13 external stream, with both the jet and external stream temperatures at 300°K. The jet exhaust was uniform and a step-like profile was employed to initiate the calculation at the nozzle exit plane. All calculations utilized a  $21 \times 21$  grid. The axial pressure gradient  $\partial P / \partial x$  was imposed to be zero in performing these calculations.

Figure 3 depicts species parameter ( $\phi$ ) contours in the two planes of symmetry for a rectangular jet problem with a 4/1 aspect ratio, showing the gradual transition towards circular jet behavior. Also depicted in Fig. 3 are near field cross flow contours (at  $x=20$ ) of the species parameter exhibiting distinct kinks in the outer mixing region. The kinks in the  $\phi$  contours are attributed to the breakdown of the initial vortex sheet surrounding the jet, with the subsequent formation of a pair of counter-rotating streamwise vortices. The vortices decay and the jet contours taken on a smooth elliptic cross-flow pattern by  $X \sim 100$ . The full paper exhibits the cross flow velocity vectors for the various cases performed, clearly exhibiting the characteristic features of the corner-induced vortex flow.



**Fig. 3 Species contours in  $Y=0$  and  $Z=0$  symmetry planes and  $X=20$  cross flow plane for subsonic rectangular jet problem.**

## Future Work

Future work is oriented towards the development of a unified model which analyzes supersonic jets exhausting into subsonic external streams. This model requires the development of an adaptive grid network which aligns the jet cross-flow sonic line with a cross-flow grid line to facilitate supersonic/subsonic coupling. The coupled problem has been solved for two-dimensional flows (Refs. 1-4) but the extension of this methodology to three-dimensional has many complexities which must be addressed (see Ref. 8).

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